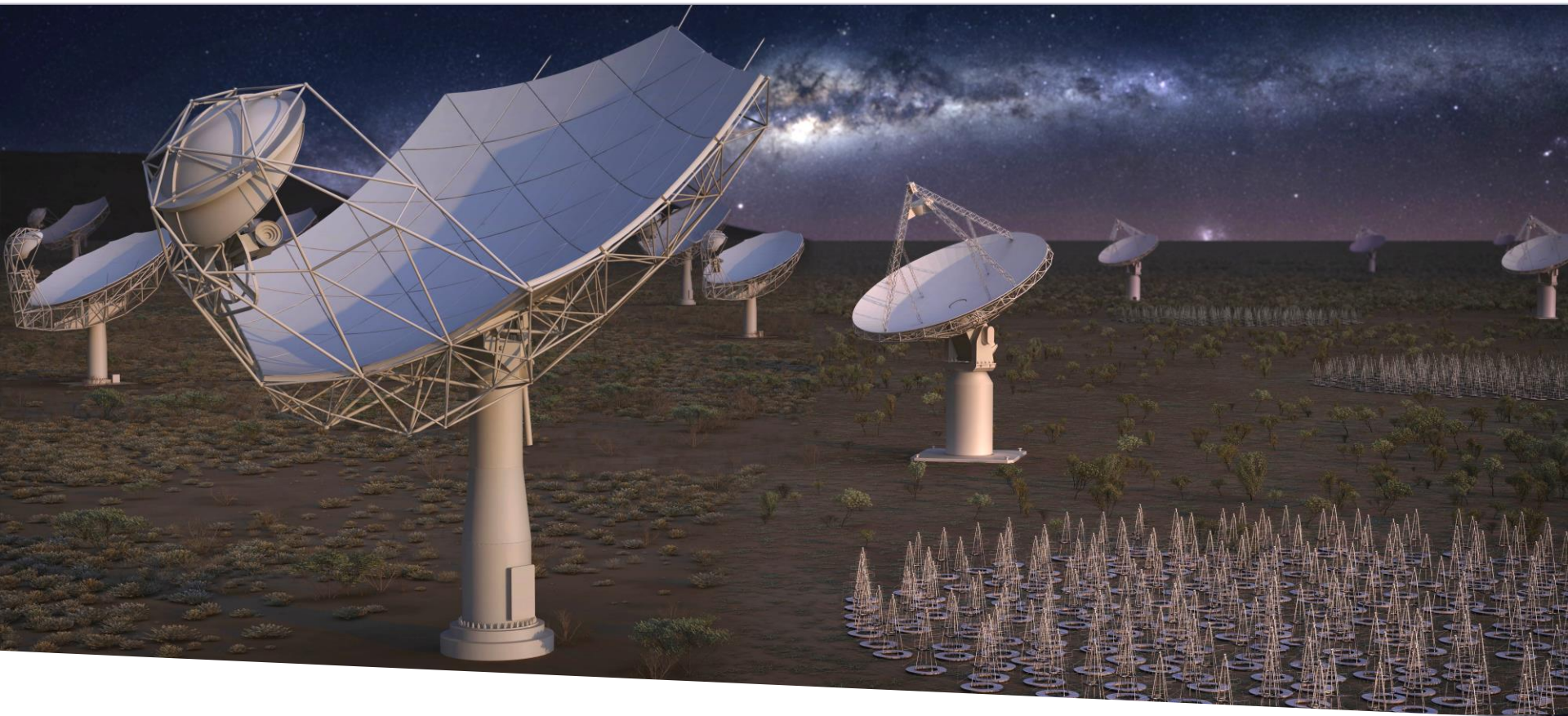


# Scientific Computing for the SKA



**SQUARE KILOMETRE ARRAY**

Exploring the Universe with the world's largest radio telescope

**Robert Braun,  
SKA Science Director**

14 February 2019

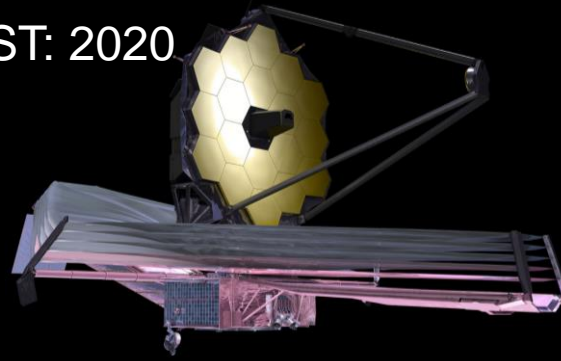


# 21<sup>st</sup> Century Observatories

LIGO: operational



JWST: 2020



ATHENA:  
2028



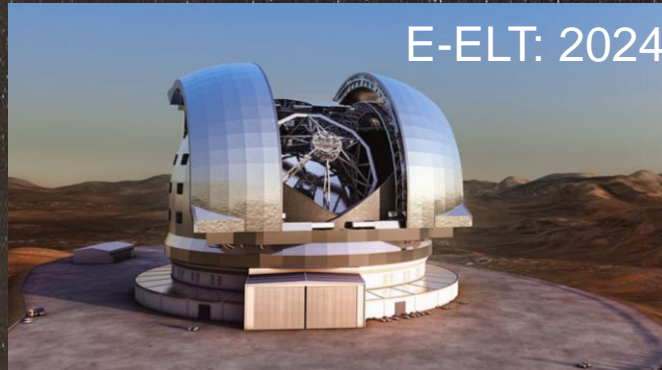
ALMA: operational



SKA: 2026



E-ELT: 2024



CTA: 2024



Radio waves

Microwaves

Infrared



Ultraviolet

X-rays

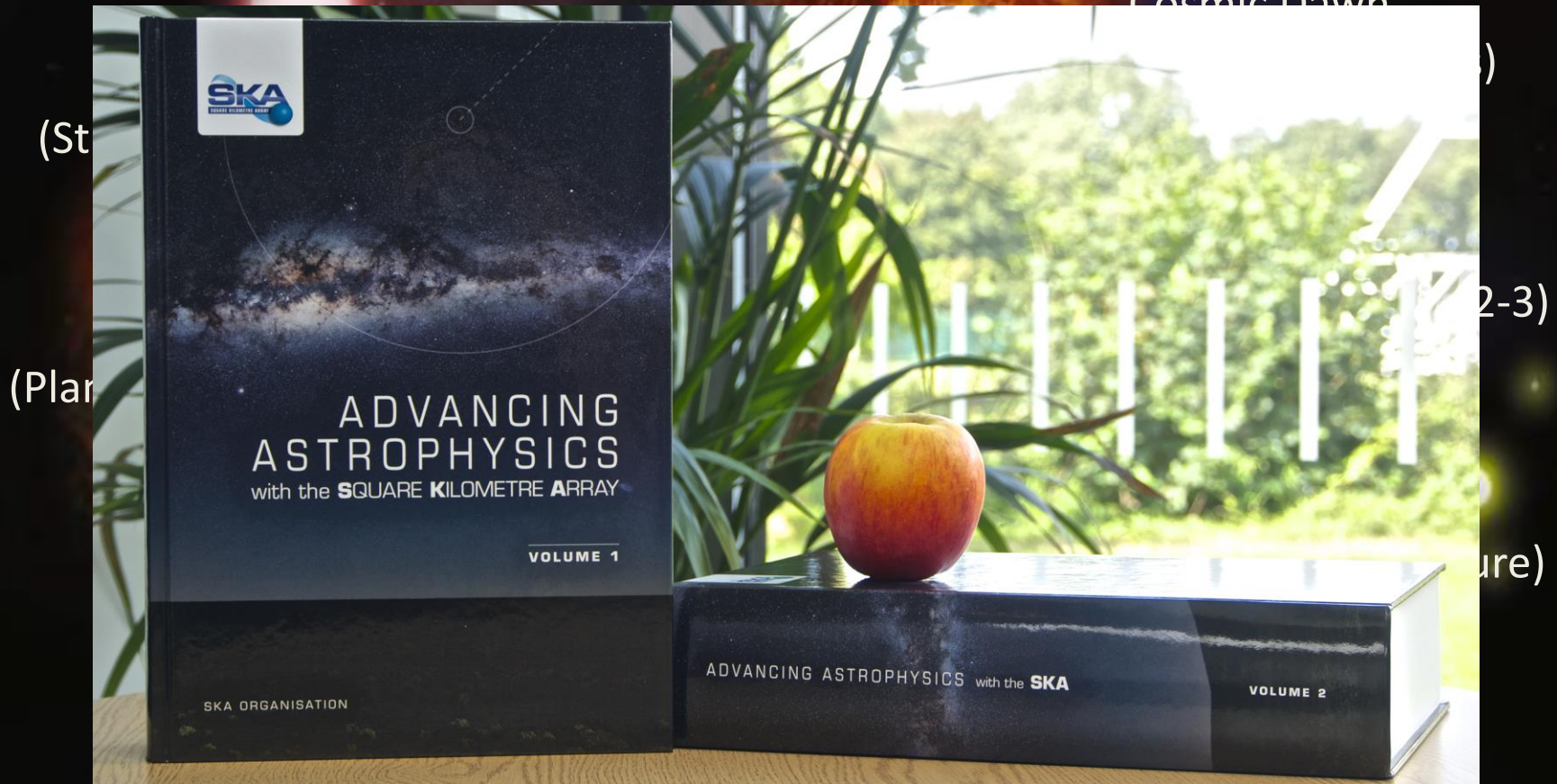
Gamma





# SKA– Key Science Drivers: The history of the Universe

Cosmic Dawn



Broadest science range of any facility on or off the Earth.

# The SKA Observatory



# SKA: A global Research Infrastructure



 **Members**  
Host Countries: Australia, South Africa, United Kingdom



Observers



 African partner countries

# SKA: A global Research Infrastructure



Current Members



Potential Future Members



 **Members**  
Host Countries: Australia, South Africa, United Kingdom



Observers



 African partner countries



# Negotiations to establish SKA Inter-Governmental Organisation.

**Text of Convention and protocols now agreed**

**Initialing of documents completed**

**Ministerial signing ceremony 12 March 2019**

**Transition planning underway**

# Square Kilometre Array

3 sites; 2 telescopes + HQ  
1 Observatory

Design Phase: ~€170M; 600 scientists+engineers

Phase 1

Construction: 2020 – 2025

Construction cost cap: €650M (2013€)

MeerKat integrated  
Observatory Development Programme

SKA Regional Centres out of scope of centrally-funded SKAO



# SKA and Big Data



# The SKA Operational Model



## 1 Observatory

The SKA

## 2 Telescopes

SKA1-LOW  
SKA1-MID

## 3 Sites

Australia (LOW)  
South Africa (MID)  
United Kingdom (GHQ)

## Principles

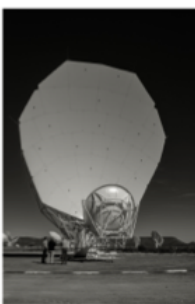
One observatory  
Optimal operation  
Minimise duplication  
Autonomy & authority



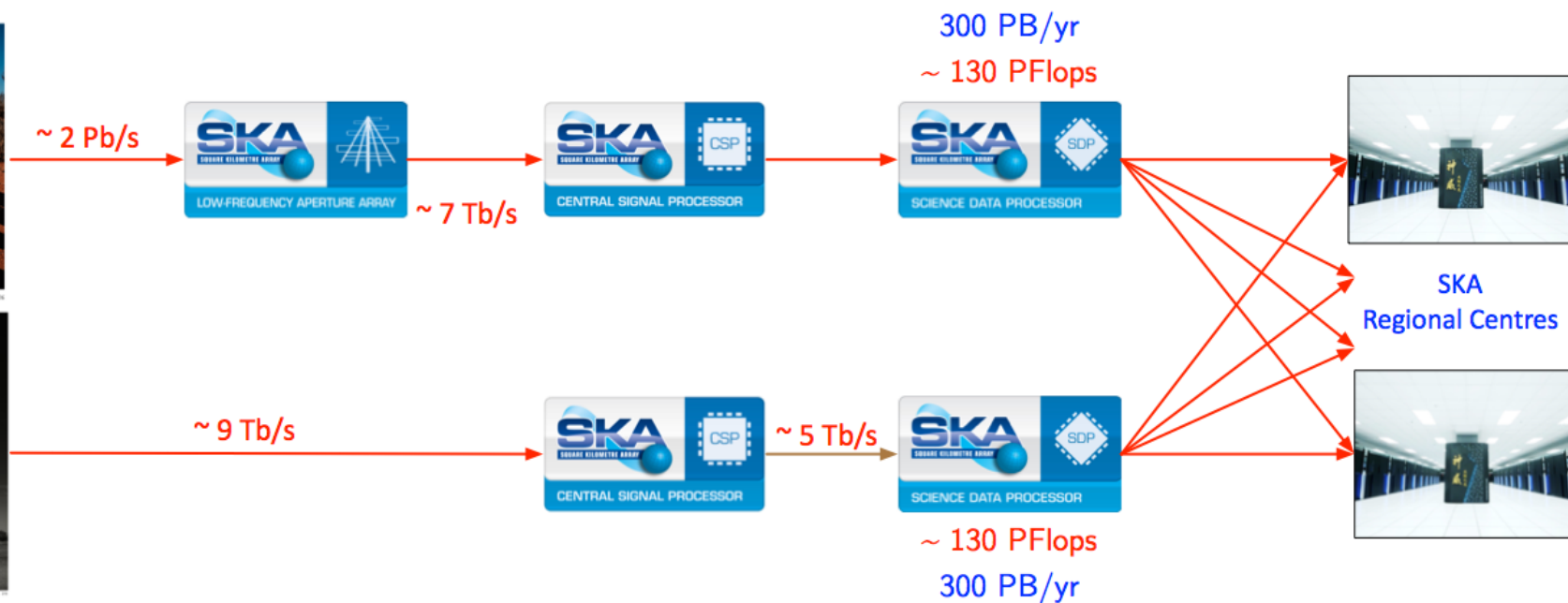


# The SKA Data Flow Challenge

SKA1-LOW

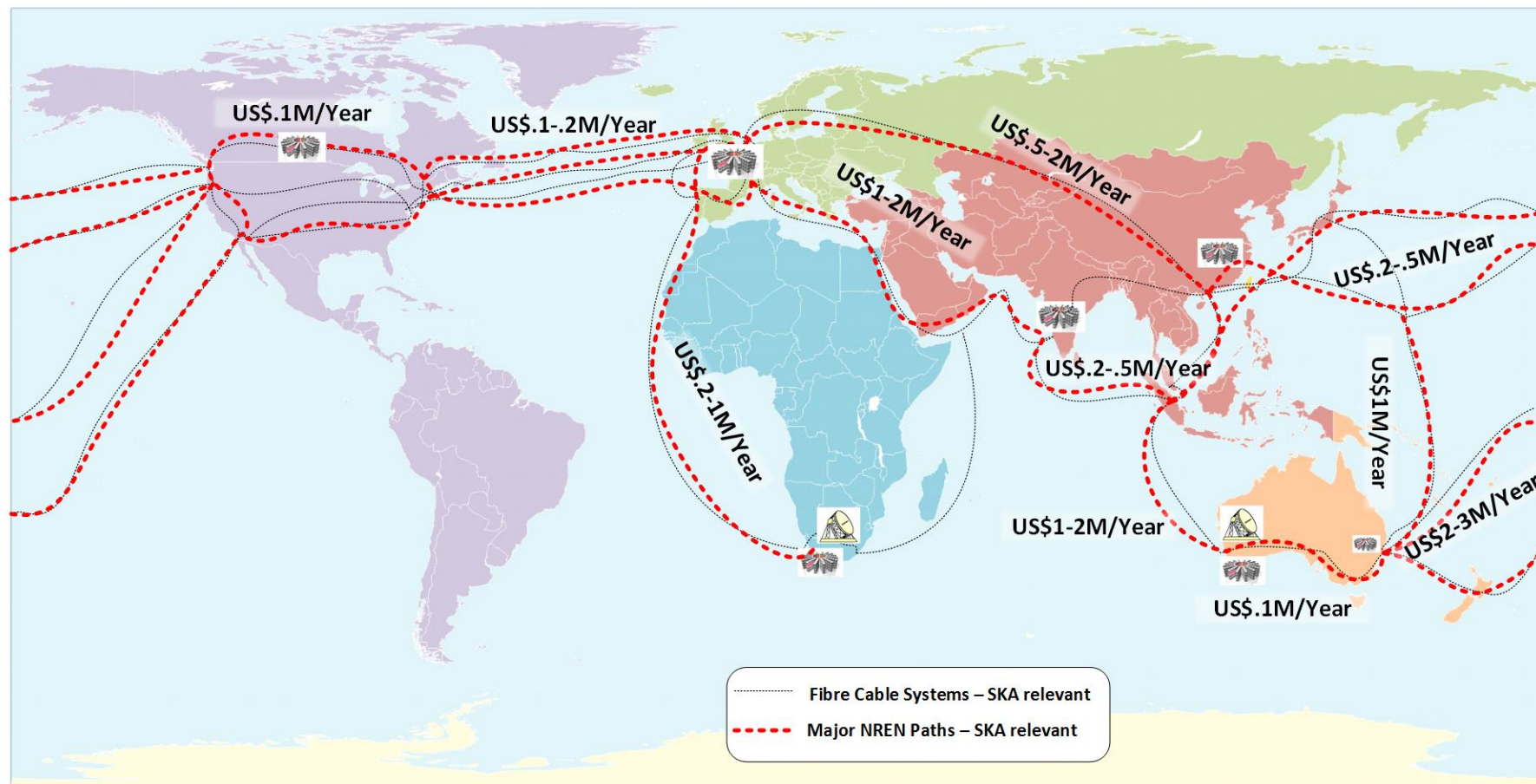


SKA1-MID



- Digital data rates are reduced by factor  $\sim 100$  within SDP via calibration and data product generation
- SDP output rate compatible with  $100 \text{ Gb/s}$  per site

# The SKA Data Flow Challenge



- Observatory Data Products flow from the Science Data Processors in Perth and Cape Town to SRCs around the globe



# The SKA Data Flow Challenge



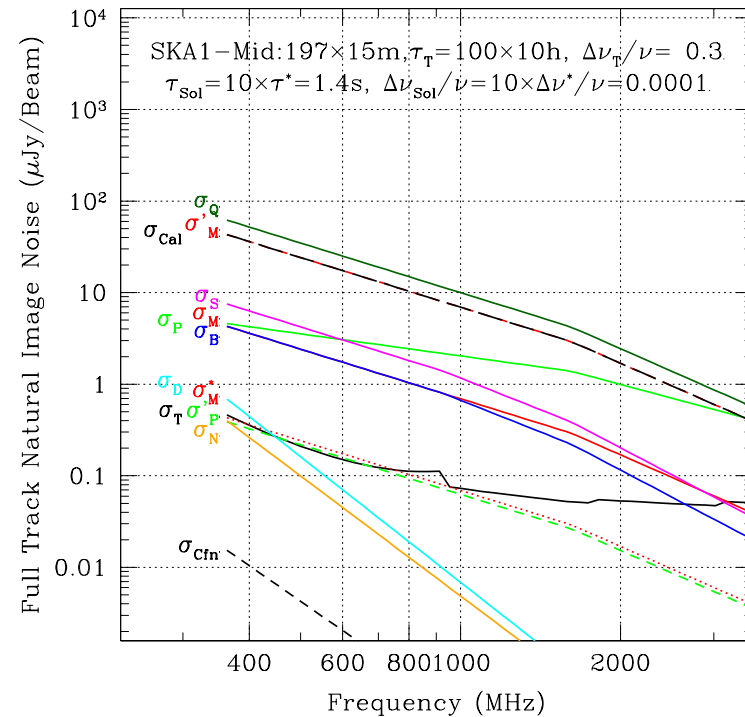
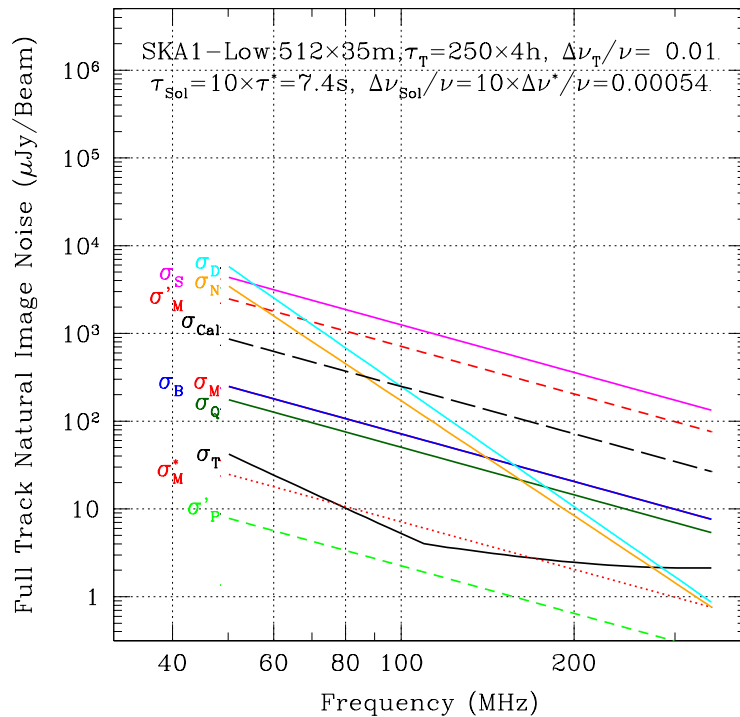
# Science Error Budgets for SKA1

| Parameter       | Definition  |
|-----------------|---|
| $\eta_F$        | Far sidelobe suppression factor                     |
| $\epsilon_F$    | Far sidelobe attenuation relative to on-axis        |
| $\epsilon_S$    | Near-in sidelobe attenuation relative to on-axis    |
| $\epsilon_M$    | Discrete source modelling error                     |
| P (arcs)        | Mechanical slowly varying systematic pointing error |
| $\tau_p$ (min)  | Timescale for slowly varying pointing error         |
| $\epsilon'_p$   | Rapidly varying random pointing induced gain error  |
| $\tau'_p$ (sec) | Timescale for rapid pointing errors                 |
| $\epsilon_Q$    | Main beam azimuthal shape asymmetry                 |
| $\epsilon_B$    | Main beam shape/gain modulation with frequency      |

- Scientific Error Budgets for SKA1-Mid and SKA1-Low (Doc #641 released)
- Small number of key instrumental and calibration parameters that determine quality of SKA data products
- Parametric model that relates each variable to a corresponding image noise for a given observational strategy
- Distribute noise degradation over all independent factors

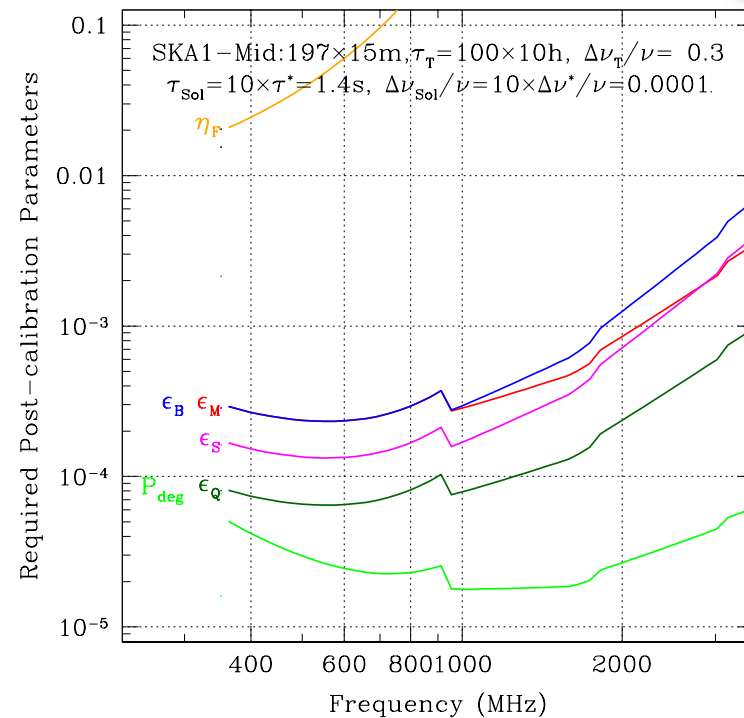
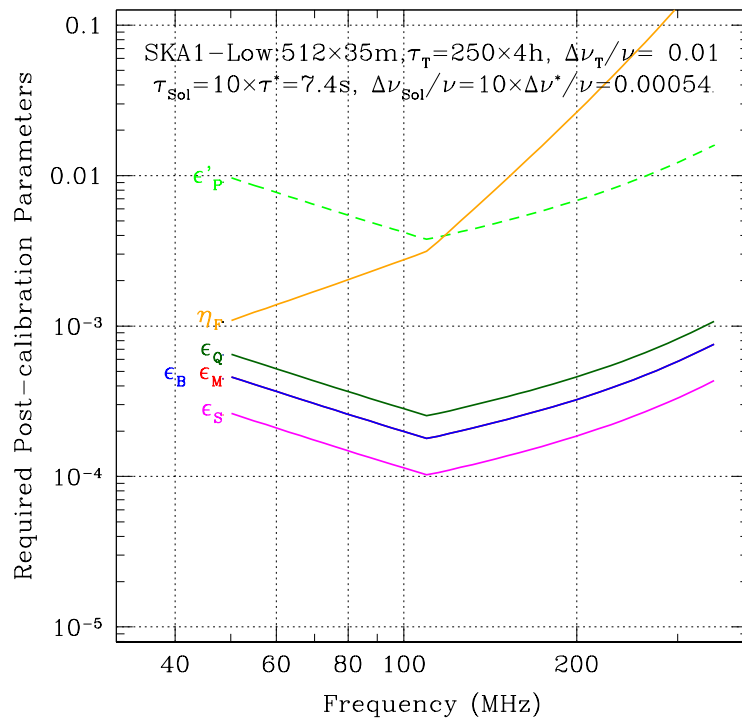


# Systematic Error Contributions for SKA1



- Individual “noise” contributions in a  $1000^{\text{h}}$  deep field
  - Pointing errors (electronic or mechanical)
  - Unmodelled sky sources in far- and near- side-lobes
  - Unmodelled beam shape and spectral gain fluctuations
  - Insufficient source modelling precision

# Systematic Error Contributions for SKA1



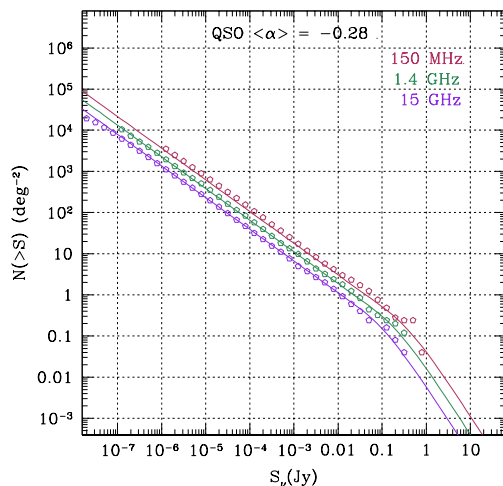
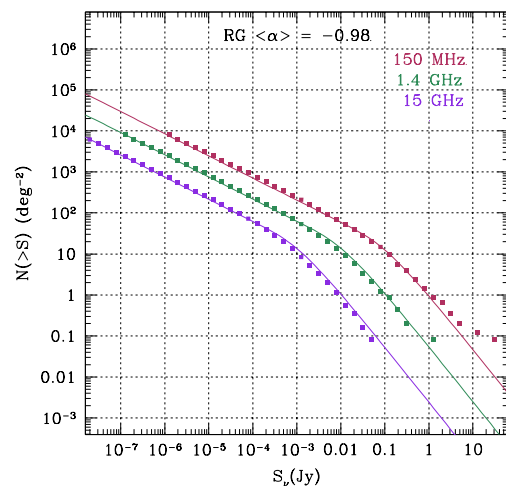
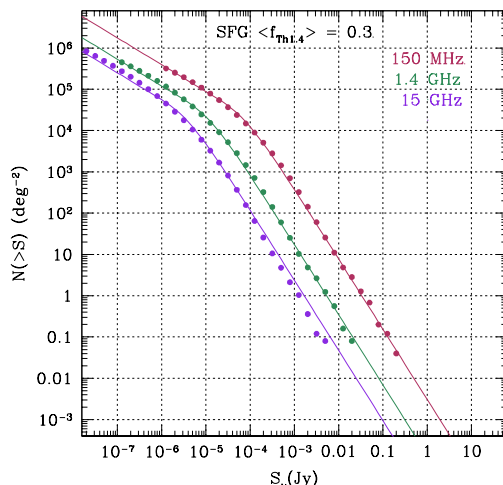
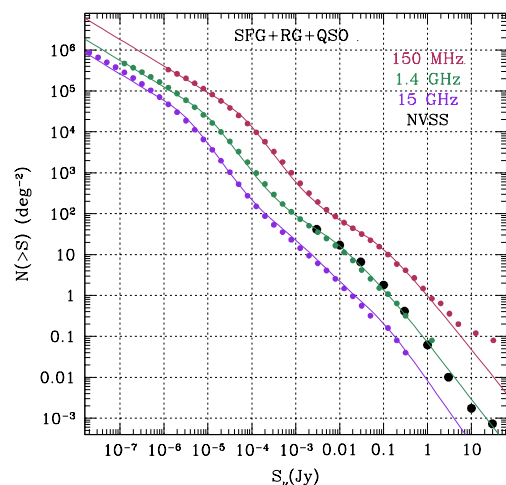
- Requirements for < 20% noise degradation in a 1000<sup>h</sup> deep field
  - Electronic pointing induced gain errors must be < -25 dB, mechanical < 0.1 arcsec
  - Unmodelled beam shape and spectral gain fluctuations must be < -40 to -35 dB
  - Precision of source modelling must exceed 35 dB
  - Brightest 4 dex of sources in main beam and near-in sidelobes must be modelled
  - Brightest 2.5 dex of all-sky sources must be modelled at lowest frequencies



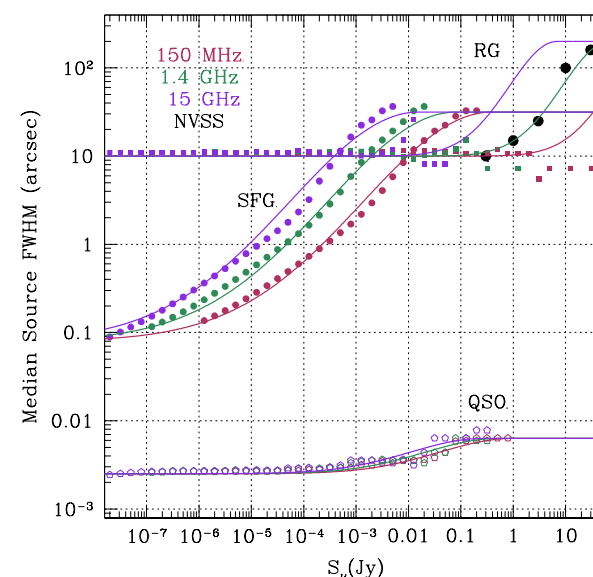
# SKA1 Calibration Requirements (Doc #941 released)

- Science Data Processor Parametric Model for SKA calibration and imaging has key parameters:
  - Use-Case Parameters:  $B_{\text{Max}}$ ,  $\nu_{\text{Min}}$  and  $\nu_{\text{Max}}$ ,  $T_{\text{Point}}$  (**total** depth for pointing)
  - Calibration Parameters: are all strong functions of ( $B_{\text{Max}}$ ,  $\nu$  and  $T_{\text{Point}}$ )
    - $N_{\text{Ateam}}$ , number of all-sky “de-mixing” sources
    - $N_{\text{Source}}$ , number of main beam and near-in side-lobe sources
    - $N_{\text{SelfCal}}$ ,  $N_{\text{Major}}$ , number of self-cal iterations, deconvolution cycles
    - $N_{\text{Ipatches}}$ , different directions requiring complex gain solution
    - $\tau_{\text{Sol}}$ ,  $(\Delta\nu/\nu)_{\text{Sol}}$ , time and frequency resolution of gain solutions
- SKAO Model for functional dependence of the Calibration parameters on the Use-case parameters
  - Celestial source number densities and sizes
  - Dish/station beam solid angle versus attenuation

# Celestial Source Models



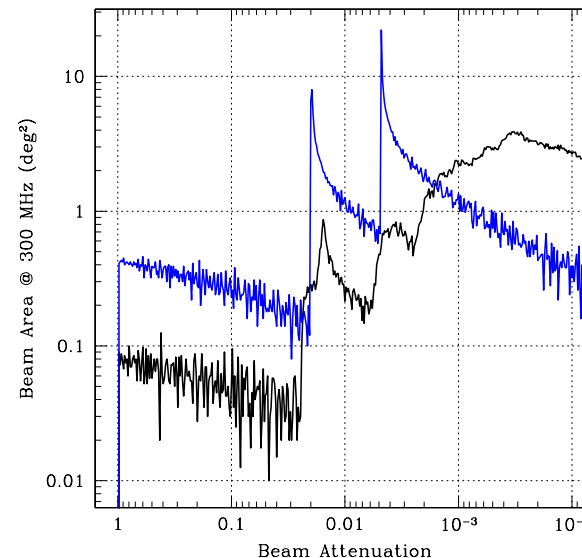
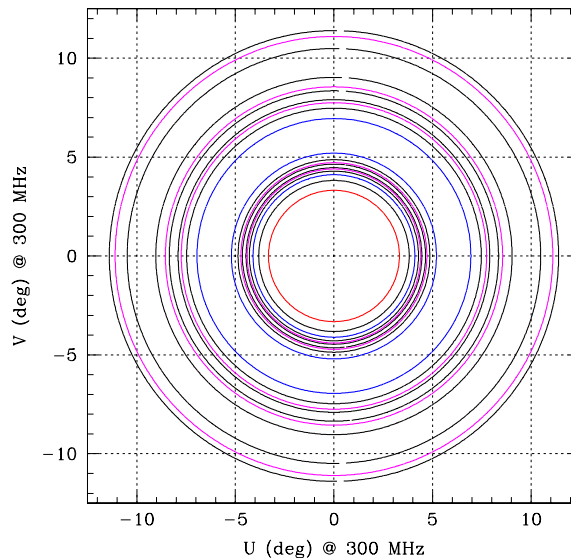
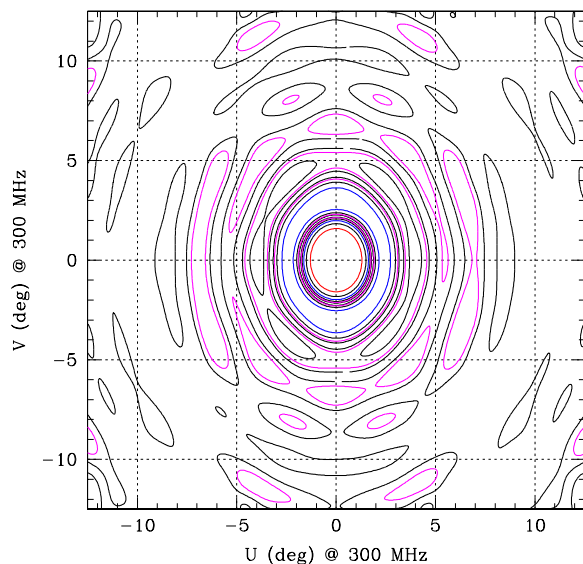
Bonaldi et al 2018,  
<https://arxiv.org/abs/1805.05222>



- Based on “T-RECS” simulation outputs at 0.15, 1.4 and 15 GHz



# Station/Dish Beam models



- Beam modelling of SKA1-Low stations and SKA1-Mid dishes for integration of source counts, including side-lobes

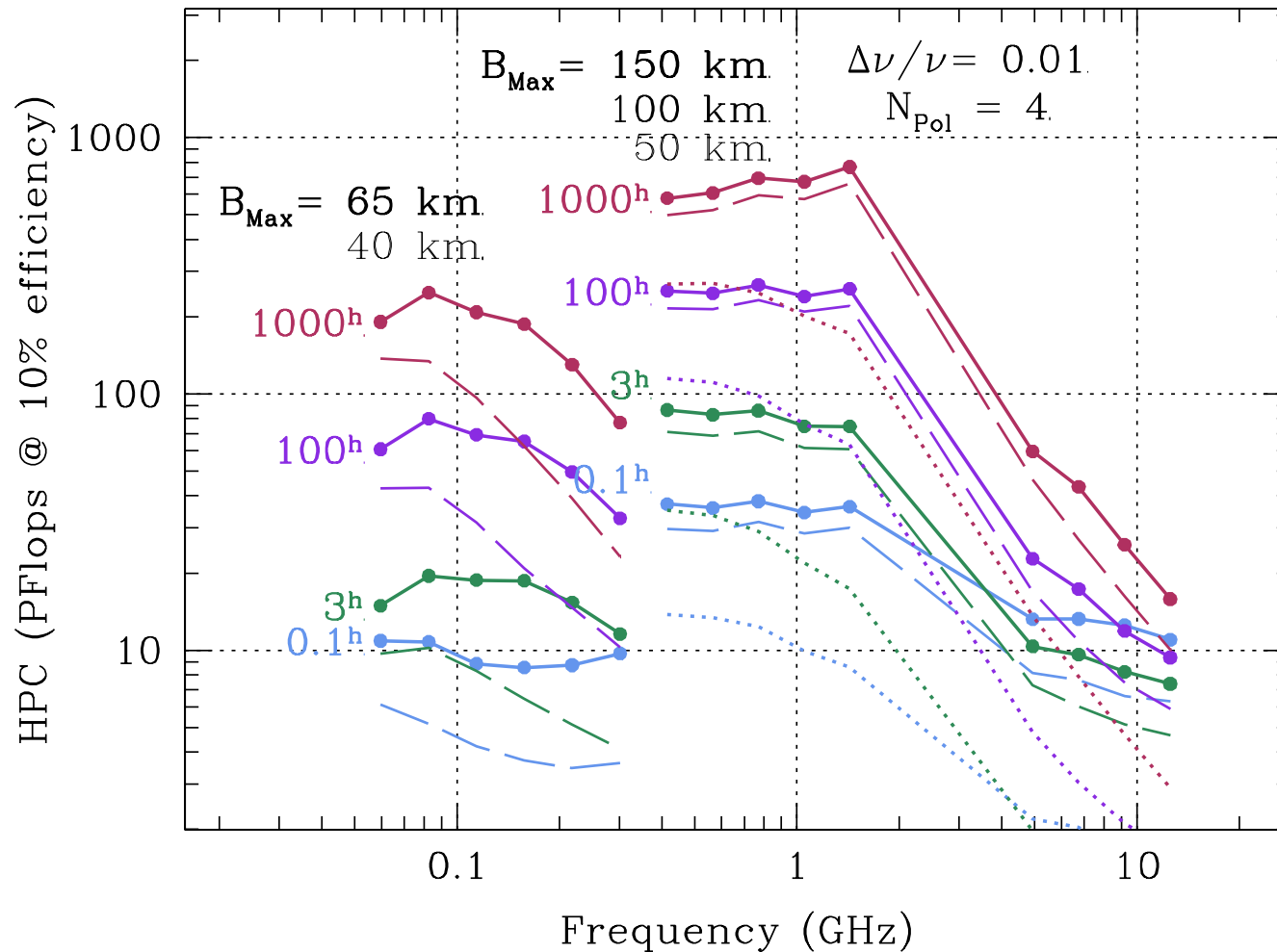
# SKA1 Calibration Strategy



| $n_{\min}$<br>(GHz) | $n_c$<br>(GHz) | $n_{\max}$<br>(GHz) | Sub-band        | Band | $N_{\text{Ateam}}$ | $N_{\text{Source}}$ | $S_{\text{Max}}$<br>(Jy) | $S_{\text{Min}}$<br>(Jy) | $N_{\text{SelfCal}}$ /<br>$N'_{\text{SelfCal}}$ | $N_{\text{Maj}}$ /<br>$N'_{\text{Maj}}$ | $N_{\text{Patch}}$ |
|---------------------|----------------|---------------------|-----------------|------|--------------------|---------------------|--------------------------|--------------------------|---|---|--------------------|
| 0.050               | 0.060          | 0.069               | Low <b>b</b> 1  |      | 19                 | 36820               | 68                       | 14m                      | 6/1   | 3/1                                     | 336                |
| 0.069               | 0.082          | 0.096               | Low <b>b</b> 2  |      | 15                 | 35270               | 32                       | 3.9m                     | 6/1   | 3/1                                     | 180                |
| 0.096               | 0.114          | 0.132               | Low <b>b</b> 3  |      | 12                 | 28390               | 14                       | 1.4m                     | 5/1   | 3/1                                     | 93                 |
| 0.132               | 0.158          | 0.183               | Low <b>b</b> 4  |      | 10                 | 24760               | 6.3                      | 0.7m                     | 5/1   | 3/1                                     | 48                 |
| 0.183               | 0.218          | 0.253               | Low <b>b</b> 5  |      | 9                  | 17050               | 2.8                      | 0.5m                     | 5/1   | 3/1                                     | 25                 |
| 0.253               | 0.302          | 0.350               | Low <b>b</b> 6  |      | 8                  | 9602                | 1.3                      | 0.5m                     | 5/1   | 2/1                                     | 20                 |
| 0.35                | 0.41           | 0.48                | Mid <b>b</b> 1  | B1   | 8                  | 29860               | 2.0                      | 0.3m                     | 6/1   | 3/1                                     | 36                 |
| 0.48                | 0.56           | 0.65                | Mid <b>b</b> 2  | B1   | 5                  | 25140               | 0.9                      | 0.1m                     | 6/1   | 3/1                                     | 20                 |
| 0.65                | 0.77           | 0.89                | Mid <b>b</b> 3  | B1   | 3                  | 21530               | 0.4                      | 60 $\mu$                 | 5/1   | 3/1                                     | 20                 |
| 0.89                | 1.05           | 1.21                | Mid <b>b</b> 4  | B2   | 2                  | 18770               | 0.2                      | 20 $\mu$                 | 5/1   | 3/1                                     | 20                 |
| 1.21                | 1.43           | 1.65                | Mid <b>b</b> 5  | B2   | 1                  | 16290               | 90m                      | 15 $\mu$                 | 5/1   | 3/1                                     | 20                 |
| 1.65                | 1.95           | 2.25                | Mid <b>b</b> 6  |      | 0                  | 11430               | 50m                      | 9 $\mu$                  | 5/1   | 3/1                                     | 20                 |
| 2.25                | 2.66           | 3.07                | Mid <b>b</b> 7  |      | 0                  | 6660                | 31m                      | 7 $\mu$                  | 5/1   | 3/1                                     | 20                 |
| 3.07                | 3.63           | 4.18                | Mid <b>b</b> 8  |      | 0                  | 3770                | 20m                      | 6 $\mu$                  | 5/1   | 3/1                                     | 20                 |
| 4.18                | 4.94           | 5.70                | Mid <b>b</b> 9  | B5a  | 0                  | 2087                | 13m                      | 5 $\mu$                  | 5/1   | 2/1                                     | 20                 |
| 5.70                | 6.74           | 7.78                | Mid <b>b</b> 10 | B5a  | 0                  | 1117                | 8m                       | 4 $\mu$                  | 4/1   | 2/1                                     | 20                 |
| 7.78                | 9.19           | 10.61               | Mid <b>b</b> 11 | B5b  | 0                  | 582                 | 5m                       | 4 $\mu$                  | 4/1   | 2/1                                     | 20                 |
| 10.61               | 12.53          | 14.46               | Mid <b>b</b> 12 | B5b  | 0                  | 293                 | 3m                       | 3 $\mu$                  | 4/1   | 2/1                                     | 20                 |

- Modelled calibration parameters that should permit ~thermal noise limited data products within very deep integrations

# SKA1 High Performance Computing Requirements



- Instantaneous HPC load as function of  $(B_{Max}, \nu, T_{Point})$



# HPC Breakdown by Use Case type



- When total HPC significant, then dominated by DFT

| Frequency (GHz) | T_Point (h) | Total HPC (Flops) | Average | Correct | De-grid | De-grid/Kernel Update | De-mix | DFT | FFT | Flag | Grid | Grid/Kernel Update | ID Comp | IFFT | Phase Out | Phase Out/Predict | Receive | Re-project | Re-project/Predict | Solve | Source Find | Subtract/Kernel Comp | Subtract/IS | Visual Weighting |
|-----------------|-------------|-------------------|---------|---------|---------|-----------------------|--------|-----|-----|------|------|--------------------|---------|------|-----------|-------------------|---------|------------|--------------------|-------|-------------|----------------------|-------------|------------------|
| 0.06            | 0.1         | 1.1               | 0       | 22      | 3       | 10                    | 5      | 27  | 0   | 0    | 3    | 10                 | 0       | 4    | 1         | 1                 | 0       | 0          | 3                  | 0     | 0           | 0                    | 0           |                  |
| 0.08            | 0.1         | 1.1               | 0       | 16      | 3       | 9                     | 6      | 33  | 1   | 1    | 3    | 9                  | 0       | 5    | 2         | 2                 | 0       | 0          | 3                  | 0     | 0           | 0                    | 0           |                  |
| 0.11            | 0.1         | 0.9               | 0       | 11      | 4       | 9                     | 8      | 33  | 1   | 1    | 4    | 9                  | 0       | 6    | 2         | 2                 | 0       | 0          | 4                  | 0     | 0           | 0                    | 0           |                  |
| 0.16            | 0.1         | 0.9               | 0       | 6       | 4       | 9                     | 9      | 38  | 1   | 1    | 4    | 9                  | 0       | 5    | 2         | 2                 | 0       | 0          | 3                  | 0     | 0           | 0                    | 0           |                  |
| 0.22            | 0.1         | 0.9               | 0       | 3       | 4       | 8                     | 12     | 43  | 0   | 1    | 4    | 8                  | 0       | 4    | 2         | 2                 | 0       | 0          | 3                  | 0     | 0           | 0                    | 0           |                  |
| 0.3             | 0.1         | 1                 | 0       | 2       | 7       | 4                     | 13     | 48  | 1   | 1    | 7    | 4                  | 0       | 4    | 0         | 0                 | 0       | 0          | 3                  | 0     | 0           | 0                    | 0           |                  |
| 0.42            | 0.1         | 3.7               | 0       | 2       | 5       | 6                     | 1      | 36  | 2   | 0    | 5    | 6                  | 0       | 10   | 6         | 6                 | 0       | 1          | 6                  | 0     | 0           | 0                    | 0           |                  |
| 0.57            | 0.1         | 3.6               | 0       | 1       | 5       | 5                     | 1      | 40  | 2   | 0    | 5    | 5                  | 0       | 10   | 6         | 6                 | 0       | 1          | 6                  | 0     | 0           | 0                    | 0           |                  |
| 0.77            | 0.1         | 3.8               | 0       | 2       | 5       | 4                     | 1      | 42  | 2   | 1    | 5    | 4                  | 0       | 10   | 6         | 6                 | 0       | 1          | 6                  | 0     | 0           | 0                    | 0           |                  |
| 1.05            | 0.1         | 3.4               | 0       | 3       | 5       | 3                     | 0      | 42  | 2   | 1    | 5    | 3                  | 0       | 10   | 6         | 6                 | 0       | 1          | 6                  | 0     | 0           | 0                    | 0           |                  |
| 1.43            | 0.1         | 3.6               | 0       | 4       | 5       | 2                     | 1      | 42  | 2   | 1    | 5    | 2                  | 0       | 10   | 5         | 5                 | 0       | 1          | 6                  | 0     | 0           | 0                    | 0           |                  |
| 4.94            | 0.1         | 1.3               | 0       | 5       | 5       | 1                     | 0      | 10  | 6   | 2    | 5    | 1                  | 0       | 30   | 3         | 3                 | 0       | 3          | 18                 | 0     | 0           | 0                    | 0           |                  |
| 6.74            | 0.1         | 1.3               | 0       | 5       | 5       | 1                     | 0      | 9   | 6   | 3    | 5    | 1                  | 0       | 30   | 4         | 4                 | 0       | 3          | 18                 | 0     | 0           | 0                    | 0           |                  |
| 9.2             | 0.1         | 1.2               | 0       | 3       | 4       | 1                     | 0      | 6   | 6   | 3    | 4    | 1                  | 0       | 32   | 5         | 5                 | 0       | 3          | 19                 | 0     | 0           | 0                    | 0           |                  |
| 12.54           | 0.1         | 1.1               | 0       | 3       | 15      | 0                     | 1      | 5   | 5   | 4    | 15   | 0                  | 0       | 28   | 0         | 0                 | 0       | 3          | 15                 | 0     | 0           | 0                    | 0           |                  |
| 0.06            | 3           | 1.5               | 0       | 16      | 2       | 8                     | 3      | 46  | 0   | 0    | 2    | 8                  | 0       | 3    | 1         | 1                 | 0       | 0          | 2                  | 0     | 0           | 0                    | 0           |                  |
| 0.08            | 3           | 2                 | 0       | 9       | 1       | 5                     | 3      | 63  | 0   | 0    | 1    | 5                  | 0       | 2    | 1         | 1                 | 0       | 0          | 2                  | 0     | 0           | 0                    | 0           |                  |
| 0.11            | 3           | 1.9               | 0       | 5       | 2       | 4                     | 3      | 68  | 0   | 0    | 2    | 4                  | 0       | 2    | 0         | 0                 | 0       | 0          | 2                  | 0     | 0           | 0                    | 0           |                  |
| 0.16            | 3           | 1.9               | 0       | 2       | 2       | 4                     | 4      | 71  | 0   | 0    | 2    | 4                  | 0       | 2    | 0         | 0                 | 0       | 0          | 1                  | 0     | 0           | 0                    | 0           |                  |
| 0.22            | 3           | 1.5               | 0       | 1       | 2       | 4                     | 6      | 68  | 0   | 0    | 2    | 4                  | 0       | 2    | 1         | 1                 | 0       | 0          | 1                  | 0     | 0           | 0                    | 0           |                  |
| 0.3             | 3           | 1.2               | 0       | 2       | 6       | 3                     | 11     | 56  | 0   | 1    | 6    | 3                  | 0       | 4    | 0         | 0                 | 0       | 0          | 2                  | 0     | 0           | 0                    | 0           |                  |
| 0.42            | 3           | 8.6               | 0       | 1       | 2       | 5                     | 0      | 49  | 1   | 0    | 2    | 5                  | 0       | 9    | 6         | 6                 | 0       | 1          | 6                  | 0     | 0           | 0                    | 0           |                  |
| 0.57            | 3           | 8.3               | 0       | 0       | 2       | 5                     | 0      | 52  | 1   | 0    | 2    | 5                  | 0       | 8    | 6         | 6                 | 0       | 1          | 5                  | 0     | 0           | 0                    | 0           |                  |
| 0.77            | 3           | 8.6               | 0       | 1       | 3       | 4                     | 0      | 53  | 1   | 0    | 3    | 4                  | 0       | 9    | 5         | 5                 | 0       | 1          | 6                  | 0     | 0           | 0                    | 0           |                  |
| 1.05            | 3           | 7.5               | 0       | 1       | 3       | 4                     | 0      | 51  | 1   | 0    | 3    | 4                  | 0       | 9    | 5         | 5                 | 0       | 1          | 6                  | 0     | 0           | 0                    | 0           |                  |
| 1.43            | 3           | 7.5               | 0       | 2       | 4       | 3                     | 0      | 52  | 1   | 0    | 4    | 3                  | 0       | 9    | 5         | 5                 | 0       | 1          | 6                  | 0     | 0           | 0                    | 0           |                  |
| 4.94            | 3           | 1                 | 0       | 7       | 10      | 3                     | 0      | 18  | 2   | 3    | 10   | 3                  | 0       | 13   | 7         | 7                 | 0       | 1          | 8                  | 0     | 0           | 0                    | 0           |                  |
| 6.74            | 3           | 1                 | 0       | 7       | 10      | 3                     | 0      | 13  | 2   | 4    | 10   | 3                  | 0       | 11   | 10        | 10                | 0       | 1          | 7                  | 0     | 0           | 0                    | 0           |                  |
| 9.2             | 3           | 0.8               | 0       | 5       | 11      | 3                     | 1      | 10  | 2   | 5    | 11   | 3                  | 0       | 11   | 12        | 12                | 0       | 1          | 7                  | 0     | 0           | 0                    | 0           |                  |
| 12.54           | 3           | 0.7               | 0       | 4       | 13      | 2                     | 2      | 8   | 2   | 6    | 13   | 2                  | 0       | 13   | 8         | 8                 | 0       | 1          | 8                  | 0     | 0           | 0                    | 0           |                  |

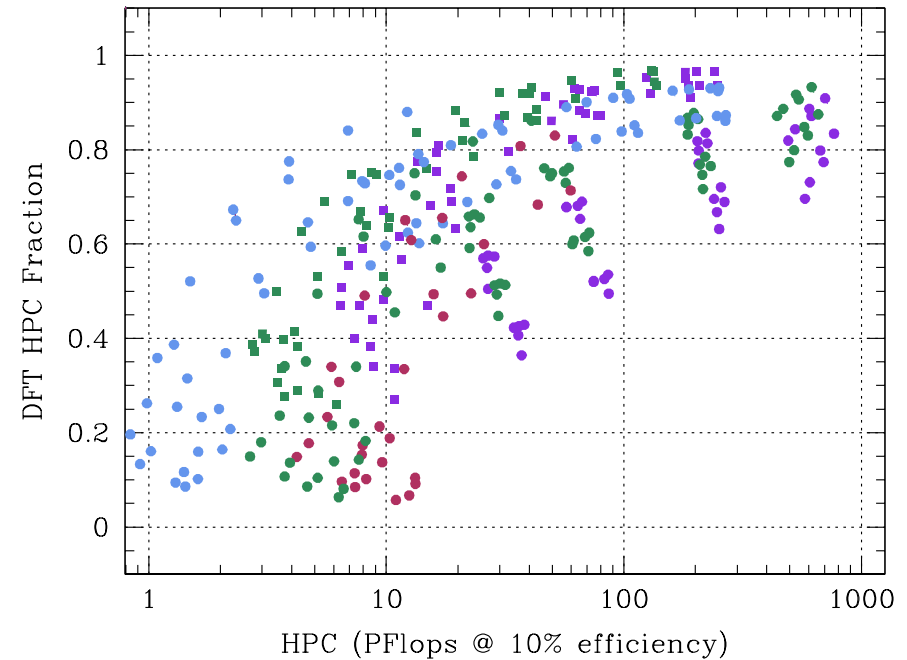
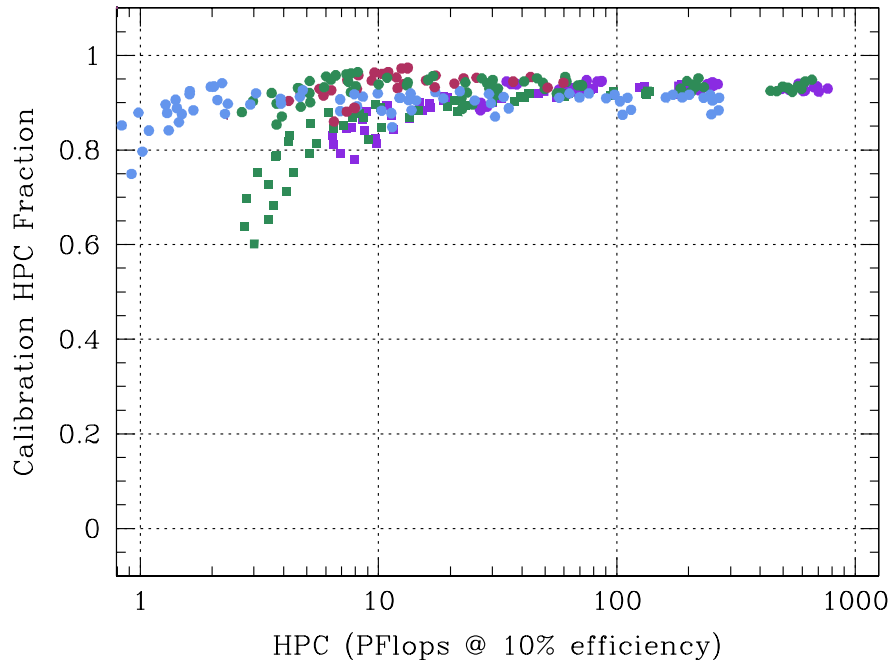
# HPC Breakdown by Use Case type



- When total HPC significant, then dominated by DFT

| Frequency [GHz] | T <sub>Point</sub> [h] | Total HPC [Flops] | Average | Correct | De-grid | De-grid kernel update | De-mix | DFT | FFT | Flag | Grid | Grid kernel update | IDComp | IFFT | PhaseRot | PhaseRot predict | Receiver | Re-project | Re-project predict | Solve | Source find | Subtract image Comp | Subtract image | VisWeighing |
|-----------------|------------------------|-------------------|---------|---------|---------|-----------------------|--------|-----|-----|------|------|--------------------|--------|------|----------|------------------|----------|------------|--------------------|-------|-------------|---------------------|----------------|-------------|
| 0.06            | 100                    | 6.1E              | 0       | 4       | 0       | 2                     | 0      | 82  | 0   | 0    | 0    | 2                  | 0      | 1    | 0        | 0                | 0        | 0          | 1                  | 0     | 0           | 0                   | 0              | 0           |
| 0.08            | 100                    | 8E                | 0       | 2       | 0       | 2                     | 0      | 87  | 0   | 0    | 0    | 2                  | 0      | 1    | 0        | 0                | 0        | 0          | 0                  | 0     | 0           | 0                   | 0              | 0           |
| 0.11            | 100                    | 6.9E              | 0       | 1       | 0       | 1                     | 1      | 87  | 0   | 0    | 0    | 1                  | 0      | 1    | 0        | 0                | 0        | 0          | 1                  | 0     | 0           | 0                   | 0              | 0           |
| 0.16            | 100                    | 6.5E              | 0       | 0       | 0       | 1                     | 1      | 88  | 0   | 0    | 0    | 1                  | 0      | 1    | 0        | 0                | 0        | 0          | 1                  | 0     | 0           | 0                   | 0              | 0           |
| 0.22            | 100                    | 5E                | 0       | 0       | 0       | 2                     | 2      | 86  | 0   | 0    | 0    | 2                  | 0      | 1    | 0        | 0                | 0        | 0          | 1                  | 0     | 0           | 0                   | 0              | 0           |
| 0.3             | 100                    | 3.3E              | 0       | 0       | 1       | 3                     | 3      | 79  | 0   | 0    | 1    | 3                  | 0      | 2    | 0        | 0                | 0        | 0          | 1                  | 0     | 0           | 0                   | 0              | 0           |
| 0.42            | 100                    | 25.2E             | 0       | 0       | 1       | 5                     | 0      | 63  | 1   | 0    | 1    | 5                  | 0      | 7    | 3        | 3                | 0        | 1          | 5                  | 0     | 0           | 0                   | 0              | 0           |
| 0.57            | 100                    | 24.7E             | 0       | 0       | 1       | 4                     | 0      | 66  | 1   | 0    | 1    | 4                  | 0      | 6    | 3        | 3                | 0        | 0          | 4                  | 0     | 0           | 0                   | 0              | 0           |
| 0.77            | 100                    | 26.5E             | 0       | 0       | 1       | 3                     | 0      | 68  | 1   | 0    | 1    | 3                  | 0      | 6    | 3        | 3                | 0        | 0          | 4                  | 0     | 0           | 0                   | 0              | 0           |
| 1.05            | 100                    | 24E               | 0       | 0       | 1       | 3                     | 0      | 69  | 1   | 0    | 1    | 3                  | 0      | 6    | 3        | 3                | 0        | 0          | 4                  | 0     | 0           | 0                   | 0              | 0           |
| 1.43            | 100                    | 25.6E             | 0       | 0       | 1       | 2                     | 0      | 72  | 1   | 0    | 1    | 2                  | 0      | 5    | 3        | 3                | 0        | 0          | 3                  | 0     | 0           | 0                   | 0              | 0           |
| 4.94            | 100                    | 2.3E              | 0       | 3       | 4       | 2                     | 0      | 49  | 1   | 1    | 4    | 2                  | 0      | 8    | 6        | 6                | 0        | 1          | 5                  | 0     | 0           | 0                   | 0              | 0           |
| 6.74            | 100                    | 1.7E              | 0       | 5       | 6       | 2                     | 0      | 44  | 1   | 2    | 6    | 2                  | 0      | 8    | 5        | 5                | 0        | 1          | 5                  | 0     | 0           | 0                   | 0              | 0           |
| 9.2             | 100                    | 1.2E              | 0       | 8       | 7       | 2                     | 1      | 33  | 1   | 4    | 7    | 2                  | 0      | 7    | 8        | 8                | 0        | 0          | 4                  | 0     | 0           | 0                   | 0              | 0           |
| 12.54           | 100                    | 0.9E              | 0       | 10      | 10      | 2                     | 1      | 21  | 2   | 5    | 10   | 2                  | 0      | 10   | 6        | 6                | 0        | 1          | 6                  | 0     | 0           | 0                   | 0              | 0           |
| 0.06            | 1k                     | 19.1E             | 0       | 1       | 0       | 1                     | 0      | 91  | 0   | 0    | 0    | 1                  | 0      | 1    | 0        | 0                | 0        | 0          | 0                  | 0     | 0           | 0                   | 0              | 0           |
| 0.08            | 1k                     | 24.8E             | 0       | 0       | 0       | 1                     | 0      | 93  | 0   | 0    | 0    | 1                  | 0      | 0    | 0        | 0                | 0        | 0          | 0                  | 0     | 0           | 0                   | 0              | 0           |
| 0.11            | 1k                     | 20.8E             | 0       | 0       | 0       | 1                     | 0      | 93  | 0   | 0    | 0    | 1                  | 0      | 0    | 0        | 0                | 0        | 0          | 0                  | 0     | 0           | 0                   | 0              | 0           |
| 0.16            | 1k                     | 18.7E             | 0       | 0       | 0       | 1                     | 0      | 93  | 0   | 0    | 0    | 1                  | 0      | 1    | 0        | 0                | 0        | 0          | 0                  | 0     | 0           | 0                   | 0              | 0           |
| 0.22            | 1k                     | 13E               | 0       | 0       | 0       | 1                     | 0      | 91  | 0   | 0    | 0    | 1                  | 0      | 1    | 0        | 0                | 0        | 0          | 0                  | 0     | 0           | 0                   | 0              | 0           |
| 0.3             | 1k                     | 7.7E              | 0       | 0       | 0       | 2                     | 1      | 87  | 0   | 0    | 0    | 2                  | 0      | 1    | 0        | 0                | 0        | 0          | 1                  | 0     | 0           | 0                   | 0              | 0           |
| 0.42            | 1k                     | 57.9E             | 0       | 0       | 1       | 4                     | 0      | 69  | 1   | 0    | 1    | 4                  | 0      | 6    | 1        | 1                | 0        | 1          | 4                  | 0     | 0           | 0                   | 0              | 0           |
| 0.57            | 1k                     | 60.7E             | 0       | 0       | 1       | 3                     | 0      | 73  | 1   | 0    | 1    | 3                  | 0      | 5    | 1        | 1                | 0        | 0          | 4                  | 0     | 0           | 0                   | 0              | 0           |
| 0.77            | 1k                     | 69.4E             | 0       | 0       | 1       | 3                     | 0      | 77  | 0   | 0    | 1    | 3                  | 0      | 4    | 1        | 1                | 0        | 0          | 3                  | 0     | 0           | 0                   | 0              | 0           |
| 1.05            | 1k                     | 67.2E             | 0       | 0       | 1       | 2                     | 0      | 79  | 0   | 0    | 1    | 2                  | 0      | 4    | 1        | 1                | 0        | 0          | 3                  | 0     | 0           | 0                   | 0              | 0           |
| 1.43            | 1k                     | 76.7E             | 0       | 0       | 0       | 2                     | 0      | 83  | 0   | 0    | 0    | 2                  | 0      | 3    | 1        | 1                | 0        | 0          | 2                  | 0     | 0           | 0                   | 0              | 0           |
| 4.94            | 1k                     | 6E                | 0       | 1       | 2       | 2                     | 0      | 71  | 1   | 0    | 2    | 2                  | 0      | 5    | 3        | 3                | 0        | 0          | 3                  | 0     | 0           | 0                   | 0              | 0           |
| 6.74            | 1k                     | 4.3E              | 0       | 2       | 2       | 1                     | 0      | 68  | 0   | 1    | 2    | 1                  | 0      | 4    | 4        | 4                | 0        | 0          | 3                  | 0     | 0           | 0                   | 0              | 0           |
| 9.2             | 1k                     | 2.6E              | 0       | 3       | 4       | 1                     | 0      | 59  | 1   | 1    | 4    | 1                  | 0      | 6    | 3        | 3                | 0        | 0          | 4                  | 0     | 0           | 0                   | 0              | 0           |
| 12.54           | 1k                     | 1.6E              | 0       | 6       | 5       | 1                     | 1      | 49  | 1   | 3    | 5    | 1                  | 0      | 6    | 6        | 6                | 0        | 0          | 3                  | 0     | 0           | 0                   | 0              | 0           |

# HPC Breakdown by Use Case type



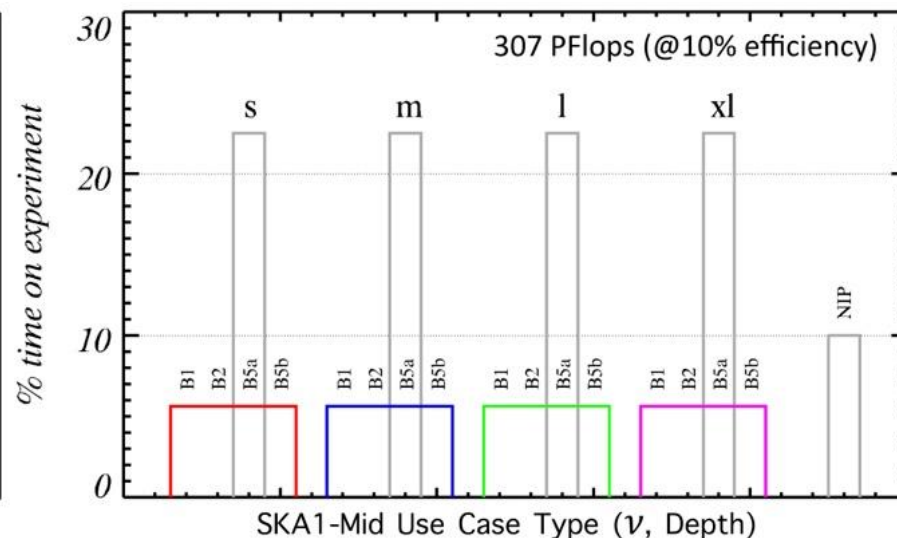
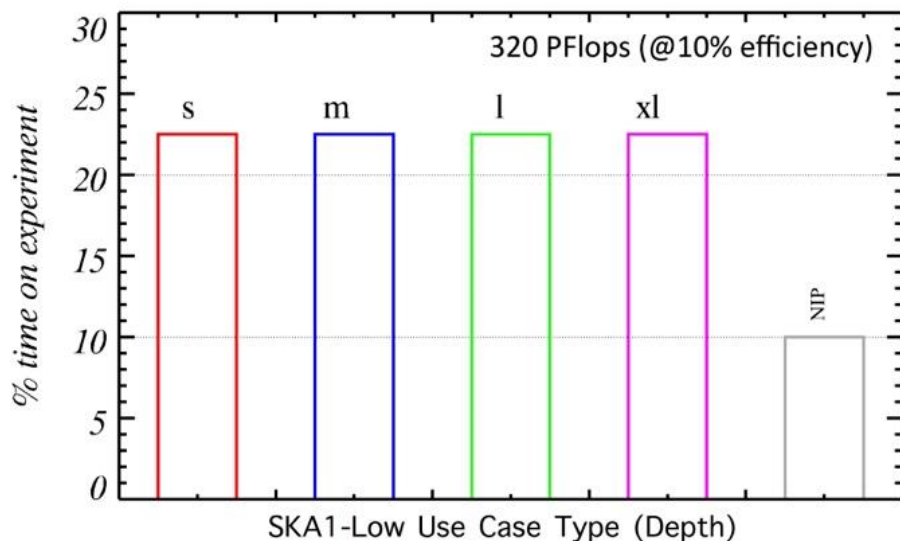
- HPC dominated by calibration, rather than data product generation
  - Implications for central HPC relative to dispersed HPC given limitations on data transmission (only highly compressed visibilities can be exported)
- HPC cost (when significant) dominated by DFT



# HPC Prediction Caveats

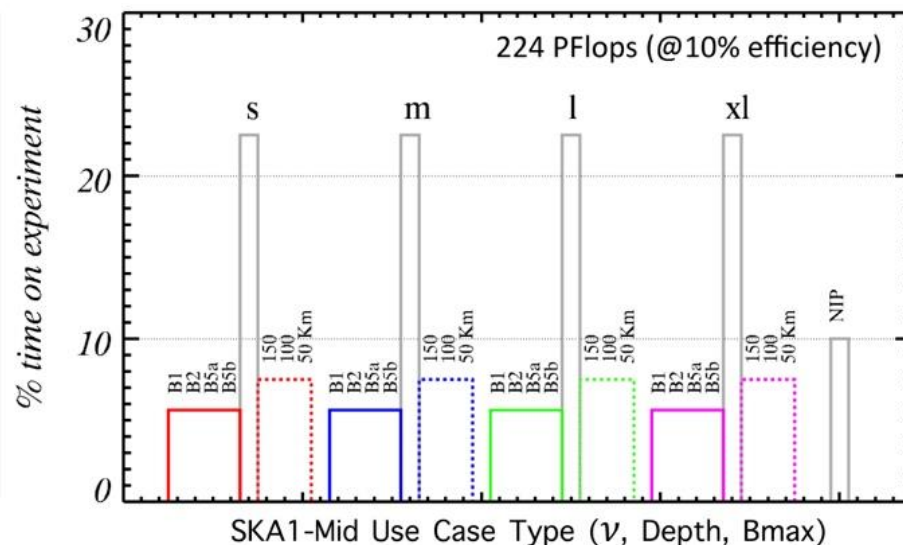
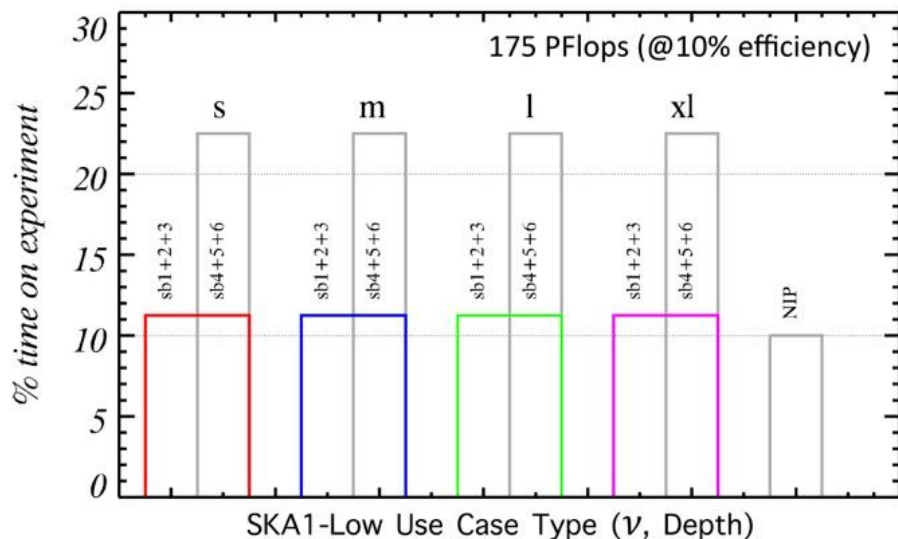
- Computational efficiency assumed to be 10%; could be much better (LOFAR EoR GPU-based pipeline achieving >80% utilisation, but smaller problem scale)
- Better representation of Direction Dependent Calibration methods needed in Parametric model
- HPC costs dominated by DFT; could be implemented with much higher than 10% efficiency (as noted above for GPUs)

# Some Use Case Distributions



- “Unconstrained Case”: 320 + 307 PFlops (@10% efficiency)
  - Process full bandwidth: 50 – 350 MHz (Low); SPF 1, 2, 5a, 5b (Mid)
  - Process at full resolution:  $B_{\text{Max}} = 65$  (Low); 150 km (Mid)
  - Uniform mix of experiment depths:  $T_{\text{Point}} = 0.1, 3, 100, 1000^{\text{h}}$

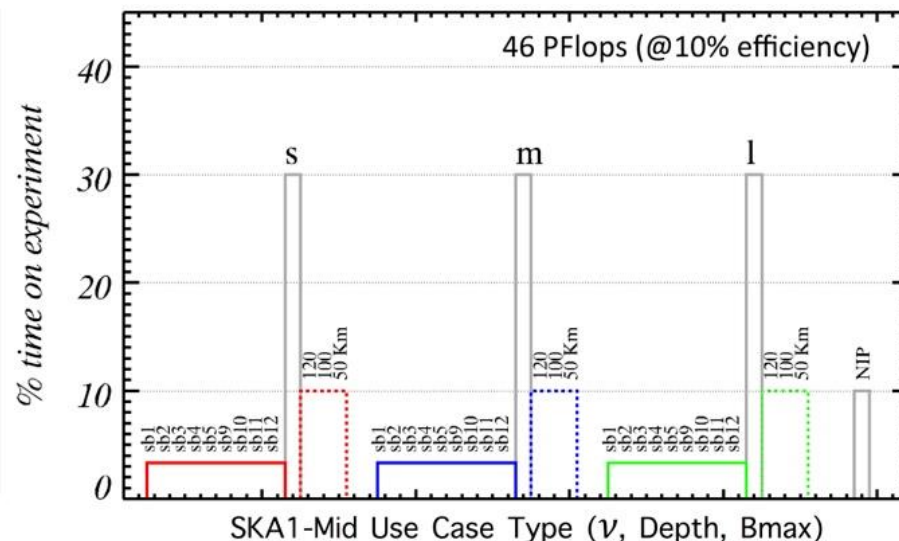
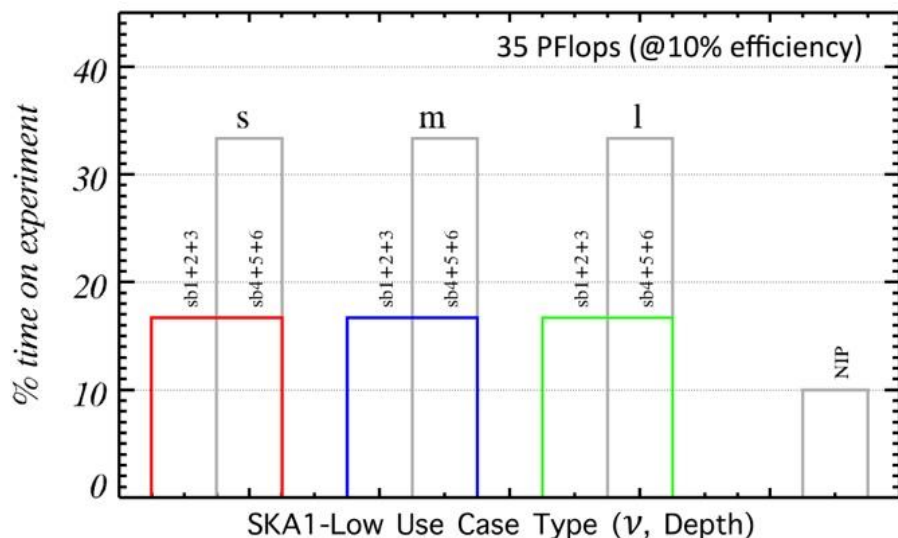
# Some Use Case Distributions



- “Constrained Case”: 175 + 224 PFlops (@10% efficiency)
  - Process bandwidth: half of 50 – 350 MHz (Low); SPF 1, 2, 5a, 5b (Mid)
  - Process at resolution:  $B_{Max} = 65$  (Low); 50, 100 or 150 km (Mid)
  - Uniform mix of experiment depths:  $T_{Point} = 0.1, 3, 100, 1000^h$

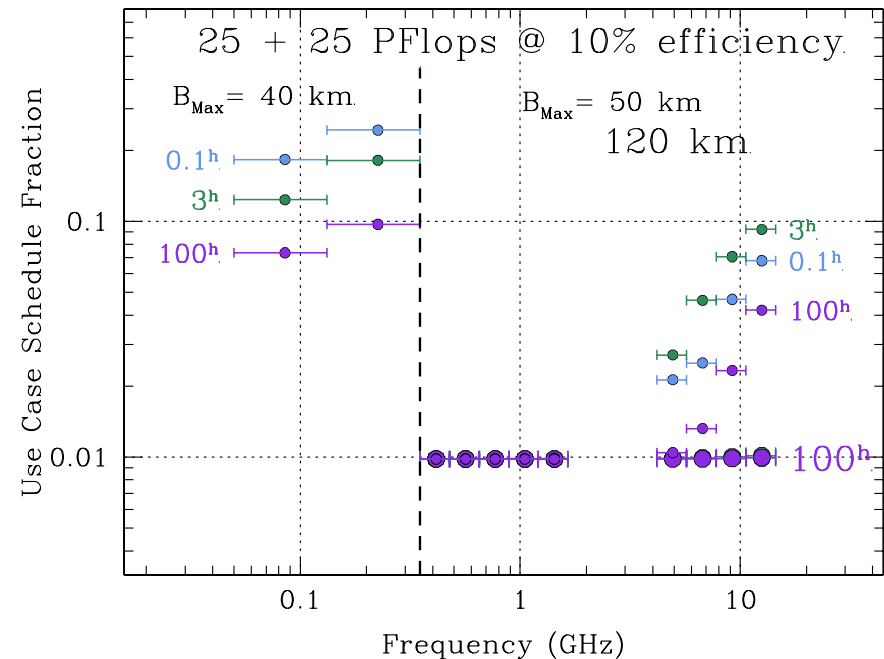
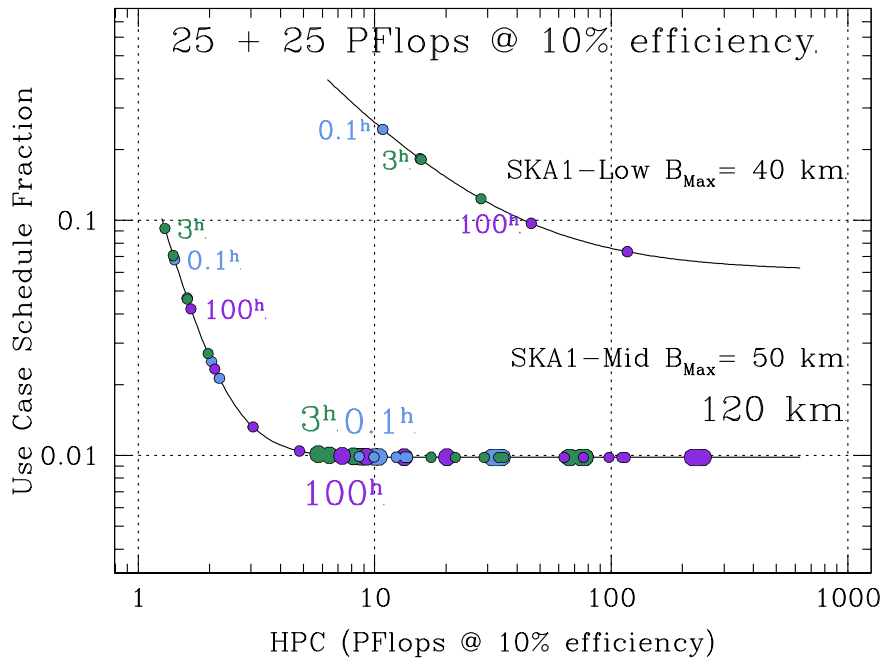


# Some Use Case Distributions



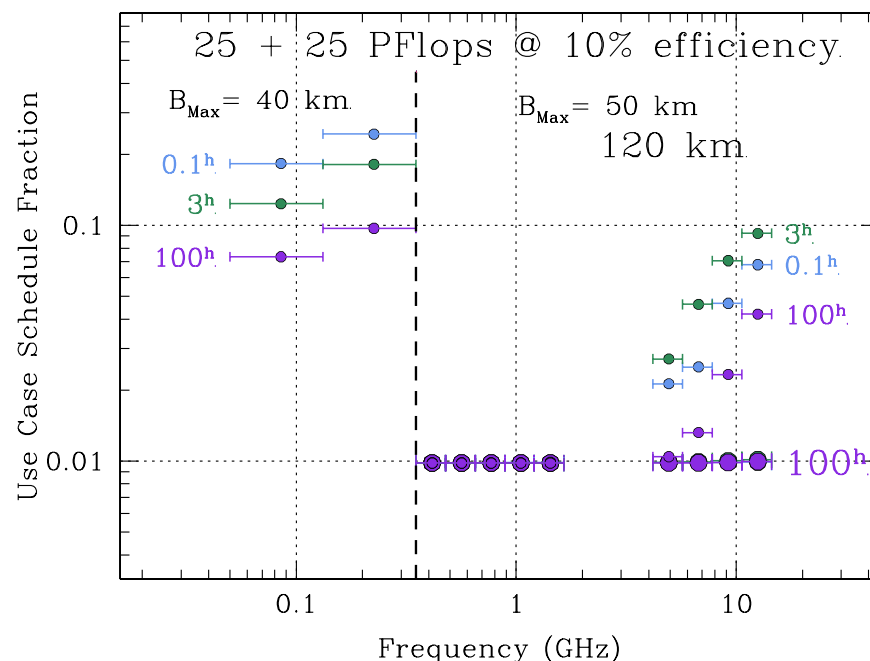
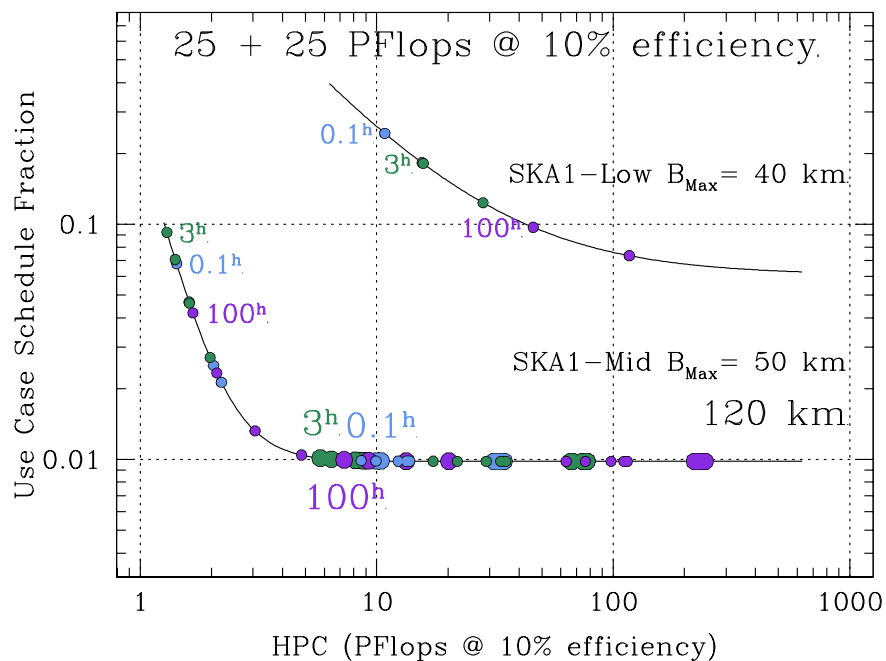
- “Highly Constrained Case”: 35 + 46 PFlops (@10% efficiency)
  - Process half band: (50 – 350 MHz)/2 (Low); (SPF 1, 2, 5a, 5b)/2 (Mid)
  - Process at resolution:  $B_{Max} = 40$  (Low); 50, 100 or 120 km (Mid)
  - Uniform mix of experiment depths:  $T_{Point} = 0.1, 3, 100^h$
  - Defer  $T_{Point} = 1000^h$

# Capped Use Case Distributions (Doc #951)



- “HPC Capped Case”: 25 + 25 PFlops (@10% efficiency)
  - Process half band: (50 – 350 MHz)/2 (Low); (SPF 1, 2, 5a, 5b)/2 (Mid)
  - Process at resolution:  $B_{Max} = 40$  (Low); 50 or 120 km (Mid)
  - Experiment depths:  $T_{Point} = 0.1, 3, 100^h$
  - Constant + Power law dependence of schedule fraction on HPC load
  - Defer  $T_{Point} = 1000^h$

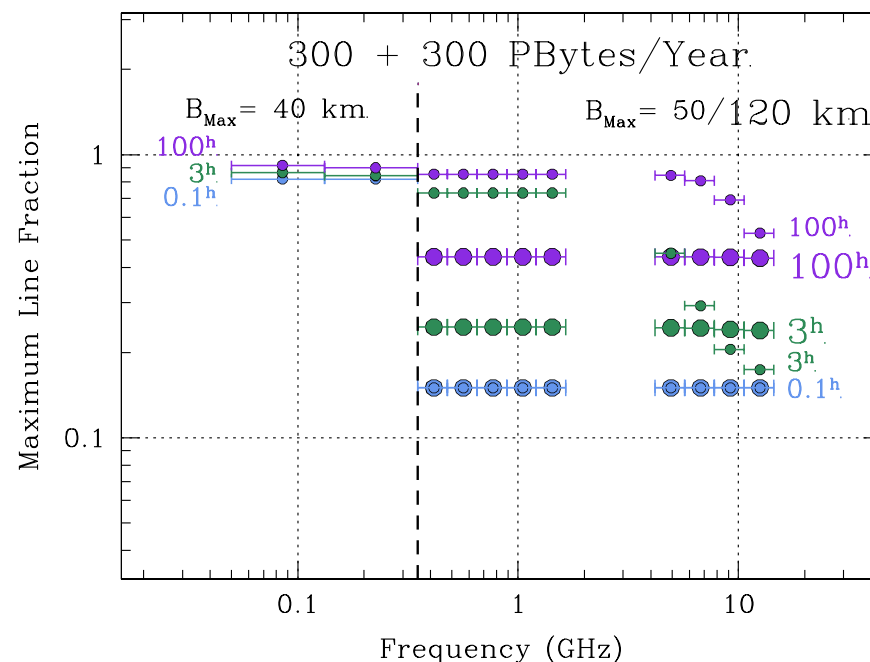
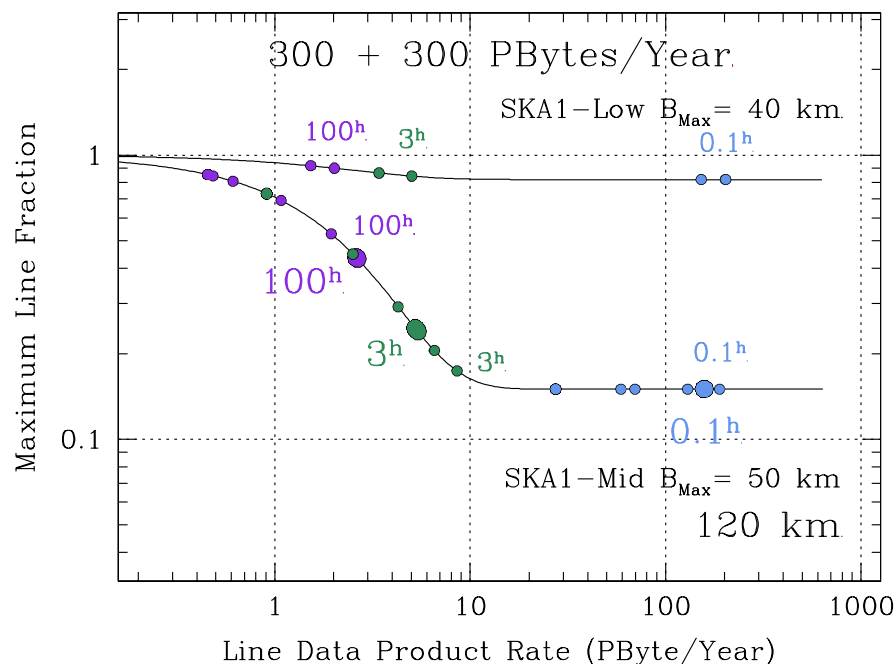
# Implications of 25 + 25 PFlops (@10 % effic.)



- Deferral of deepest integrations:  $T_{Point} \approx 1000^h$
- Loss of simultaneity from half bandwidth
- Relatively low scheduling fractions for 0.35 – 1 GHz (about half “uniform”)
- High scheduling fractions for > 5 GHz used to provide load balancing



# Implications of 25 + 25 PFlops (@10 % effic.)

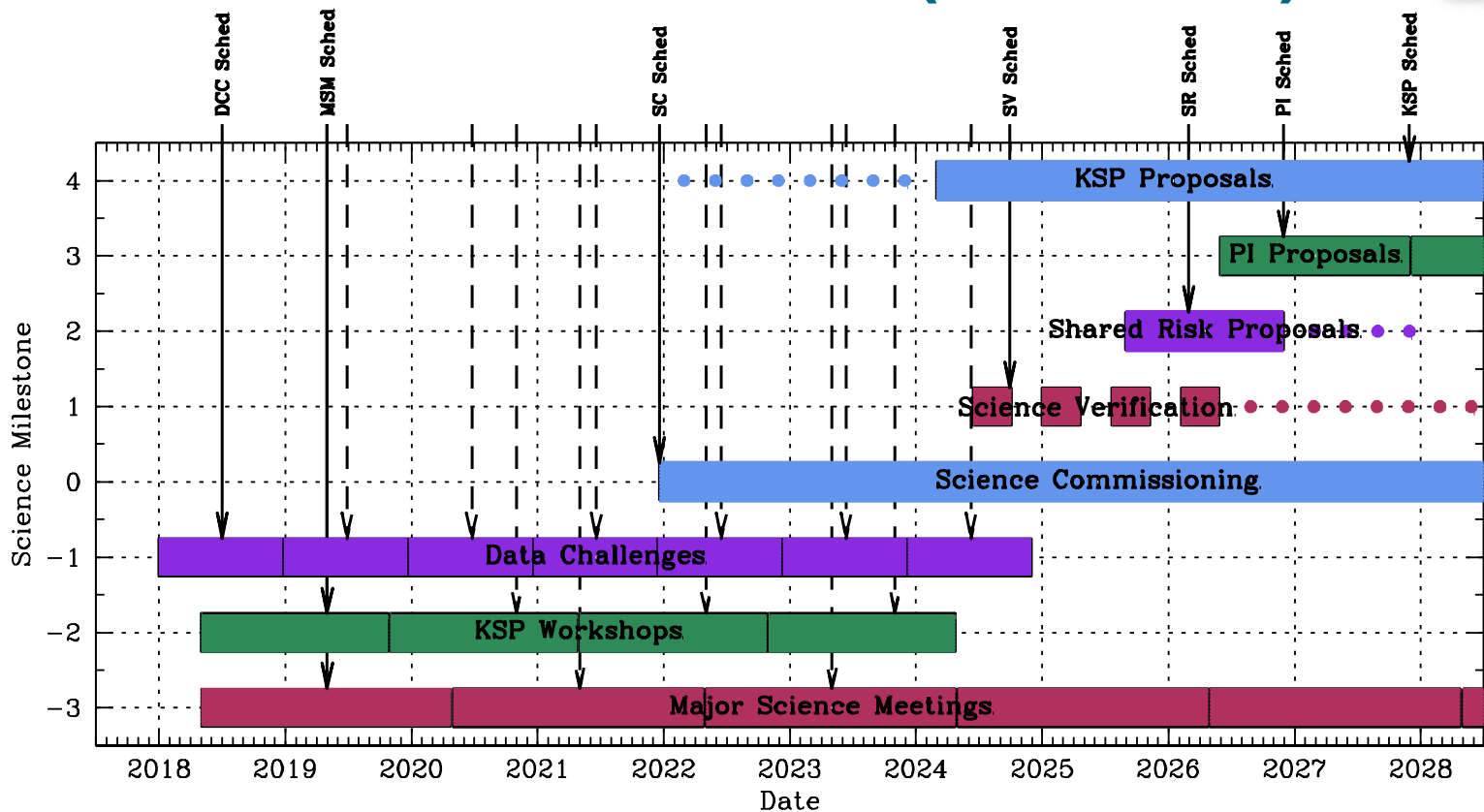


- **Archive Constraints: 300 + 300 PBytes / Year**
  - Adopt schedule fractions from Capped HPC = 25 + 25 PFlops scenario
  - Limits on spectral-line fraction imposed by 100 Gb/s per telescope link
  - Constant + exponential dependence of spectral-line fraction on Data Product Rate
  - Only mild constraints on SKA1-Low
  - Strong constraints on short observations with SKA1-Mid imposed by link speed

# Desired HPC, Network and Archive Capacity

- HPC of  $\sim 30 + 30$  Effective PFlops (@100% efficiency) would provide full bandwidth and good use case mix
  - Vital to co-design software and hardware tuned to eliminate bottlenecks
- Data transport
  - SKA1-Low: 1 – 2 x 100 Gb/s
  - SKA1-Mid: 5 – 10 x 100 Gb/s
- Archive
  - SKA1-Low: 300 – 600 PB/yr
  - SKA1-Mid: 1500 – 3000 PB/yr

# SKA1 Science Milestones (Doc #822)



- Overview of preparatory and scientific observing activities
- KSP Preparatory Activities
  - Pilot surveys in Shared-risk and PI Proposal Cycles
  - Commissioning data to facilitate survey and pipeline design

# SQUARE KILOMETRE ARRAY

Exploring the Universe with the world's largest radio telescope

